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## OPTICAL INTERFACE UNIT

This invention generally relates to optical interface units, and specifically to an optical interface unit for coupling an optoelectronic device such as a transmitter, receiver, or transceiver to a fiber stub array, and the combination to a conventional fiber optic connector.

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## CROSS-REFERENCE TO RELATED APPLICATION

The present application claims the benefit of U.S. provisional patent application No. 60/251,149, filed December 4, 2000, the contents of which are hereby expressly incorporated herein by reference.

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## BACKGROUND

Optical fiber technology is used in a variety of applications such as telecommunication, computer, and medical applications. The basic elements included in an optical data communications system include a transmitter, optical cable with connectors, and a receiver. The transmitter converts the electrical signal to a light signal that travels through the optical cable to the receiver. The receiver converts the optical signal back into an electrical signal.

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The light receiving and emitting ends of the optical fibers are housed in fiber ferrules. The fiber ferrule at the light receiving end of the bundle is coupled to a light detecting device via an optical interface unit. Likewise, the fiber ferrule at the light emitting end of the bundle is coupled to a light emitting device via an optical interface unit.

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Several optical interface technologies and consortiums have evolved that provide a standardized interfaces between two optical fiber cables, however, such standardized interfaces do not necessarily provide solutions for the coupling of light between a fiber and an optoelectronic device.

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## SUMMARY

In an exemplary embodiment of the present invention, an optical interface unit axially aligns the core of a fiber with an optoelectronic device and interfaces that combination fiber and optoelectronic device to a standardized optical connector. The optical interface unit may be

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1 optimized to interface with a particular Optical Sub-Assembly design so as to maximize optical  
coupling between the optoelectronic device and the fiber. In addition, the optical interface device  
further provides a standardized interface for visible contact connection between the various fiber  
5 stubs on the interface unit and the terminated fibers in the standardized connector (which, as  
discussed below, are generally MT/MPO ferrules attached to fiber ribbon or cable).

## BRIEF DESCRIPTION OF THE DRAWINGS

10 These and other features, aspects, and advantages of the present invention will become  
better understood with regard to the following description, appended claims, and accompanying  
drawings where:

15 FIG. 1 is an isometric view of an interface unit according to the present invention in an  
assembled configuration;

20 FIG. 2 is an exploded isometric view of the embodiment of FIG. 1;

25 FIG. 2A is a reversed isometric view of an optoelectronic plate of FIG. 2;

30 FIG. 3 is an isometric view of the embodiment of FIG. 1 in a semi-assembled  
configuration;

35 FIG. 4 is a cut-away side plan view of the embodiment of FIG. 1;

40 FIG. 5 is an isometric view of an alternative fiber stub array.

45 FIG. 6 is a reverse isometric view of the alternative embodiment of FIG. 5;

50 FIG. 7 is an exploded isometric view of an alternative interface unit;

55 FIG. 8 is an isometric view of half of a two-part alternative fiber stub array;

60 FIG. 9 is an isometric view of the other half of the two-part alternative fiber stub array  
of FIG. 8;

65 FIGS. 10-13 are various isometric views of another exemplary fiber stub array  
embodiment;

70 FIGS. 14-16 are various isometric views of yet another fiber stub array embodiment;

75 FIG. 17 is an exploded isometric view of a portion of another connector unit  
embodiment;

1 FIG. 18 is an isometric view of an exemplary optoelectronic plate mounted to a flex  
circuit;

5 FIG. 19 is an isometric view of the embodiment of FIG. 17 in an assembled state;

10 FIG. 20 is a front plan view of the cradle of FIG. 17;

15 FIG. 21 is a top plan view of the cradle of FIG. 17;

FIGS. 22-24 are various plan views of the wedge of FIG. 17;

FIGS. 25 and 26 are plan views of yet another fiber stub array embodiment;

10 FIG. 27 is an exploded view of the exemplary optoelectronic plate of FIG. 18;

FIG. 28 is an alternative embodiment of the optoelectronic plate of FIG. 18;

15 FIG. 29 is an exploded isometric view of yet another alternative interface unit;

FIG. 30 is an exploded isometric view of yet another alternative interface unit;

20 FIG. 31 is an isometric view of a portion of the interface unit of FIG. 30 from a another  
perspective; and

25 FIG. 32 is an isometric view of the alternative interface unit of FIG. 30 rotated 180  
degrees and in an assembled state with a VCSEL plate subassembly.

## 20 DETAILED DESCRIPTION

There is therefore provided according to an exemplary embodiment of the present invention, an optical interface unit for interfacing with an array of semiconductor lasers, such as for example, vertical cavity surface emitting lasers (VCSELS). Referring to FIG. 1, an exemplary optical interface unit 10 provides an interface between an optoelectronic device (not shown) and industry standard MT/MPO connectors (not shown). In broad terms, the optical interface unit 10 axially aligns the core of a fiber with the optoelectronic device and interfaces that fiber/optoelectronic combination to an industry standard connector. This is a particularly challenging task because the light-carrying region (the core) of the optical fiber can be quite small and alignment between that region and the other components (e.g., VCSEL) require extreme accuracy to efficiently transmit/receive electrical signals. In single-mode optical fibers, for example, the core diameter of each fiber is about eight microns, and the laser to fiber alignment is typically required to be within +/- 0.5-1 micron.

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1        In one embodiment of the present invention, the optical interface unit 10 further provides  
mechanical stability and protection to the interface between the standardized connector and the  
5        optoelectronic device in its working environment. This is achieved in part by ensuring low  
insertion loss in coupling a single mode fiber to an optoelectronic device housed in an Optical  
10      Sub Assembly (OSA). Among several possibilities, this is carried out by ensuring proper axial  
alignment between the fiber and the optoelectronic device, setting an appropriate gap between  
the fiber and the optoelectronic device, and checking the optical surface conditions of either the  
15      fiber or the OSA for acceptable tolerances. Persons of ordinary skill in the art will appreciate that  
if adequate alignment or assembly is not achieved, this may result in reflection problems, fiber  
tilt issues, and erroneous air gaps between the optoelectronic device and the fiber stub array  
("FSA"), and between the FSA and the fibers in the conventional connector. Stability and  
20      junction protection is generally a function of connector design (e.g., minimization of the different  
thermal expansion and mechanical movement effects), which this interface unit intended to  
achieve.

25      Advantageously the optical interface unit may be designed to interface with a particular  
OSA design so as to optimize the interface gap for the desired medium (e.g., air, epoxy, etc.).  
Hence, while described with specificity for coupling to a conventional MTP/MPO connector, the  
30      interface unit may be modified to fit other connectors without deviating from the scope of the  
present invention, such as by modifying the gap, type of slope, etc. In addition, the optical  
interface unit further provides a standardized interface for optical coupling between the  
individual fiber stubs and the terminated fibers in the standardized connector. The optical  
35      interface unit therefore maximizes coupling between an optoelectronic device and the  
standardized connector.

FIG. 2 illustrates an exemplary optical interface unit assembly 10 for interfacing a  
30      VCSEL array 12 with a MTP/MPO connector latch 14. In this embodiment the optical interface  
unit 10 includes a cradle unit 16 having a lower cradle member 17 and a cradle cover 18. The  
lower cradle 17 and cover 18 are configured to encase a FSA or array block 20 and to  
mechanically couple to a conventional MTP/MPO connector latch 14 on one side, and to a two-  
part VCSEL plate assembly 22 on the other.

1        The two-part VCSEL plate assembly 22 includes an upper ceramic substrate 24 and a  
lower metallic plate 25. The upper substrate 24 of this embodiment is configured to accept a  
monitor diode 26 positioned thereon to monitor optical output from a bi-directional emitting  
5        VCSEL array 12 and to send the monitored output to a controller or some other interface unit to  
regulate the laser output. As further discussed below, the monitor diode 26 is placed such that  
when the upper substrate 24 and the lower plate 25 are mated (such as with passive alignment  
10      equipment using a pick and place device), the monitor diode 26 is positioned subjacent to one  
of the VCSELs and in-line with a monitoring notch 28. The notch 28 is centrally located on the  
metal plate 25.

15      In detail, the lower cradle 17 has a generally U-shaped configuration and, in one  
embodiment, may be made of a weldable material such as stainless steel, Kovar, and Invar. The  
cradle is manufactured with two vertical support arms 30 and threaded hold-down aperture 32  
on each arm. The lower cradle 17 is further configured with a stepped deck 34, created in part  
by disposing two generally square steps 36 on the deck's two ends and a step guide 38 on one of  
the two edges. The steps 36 abut the vertical support arms 30 on one side and are proximate to  
the first mating surface 44 on another. Between the steps 36 is a narrow channel, which defines  
20      a notch 42. The steps 36 extend opposite the first mating surface 44 and terminate shy of a  
second mating surface 46. As further discussed below, this creates a landing 48, which is located  
near the step guide 38, and both the landing and the step guide are in the general vicinity of the  
second mating surface 46. As further discussed below, the notch 42 and the step guide 38 work  
25      in tandem to create a close tolerance fit with the FSA 20 when the FSA 20 is encased between  
the lower cradle 17 and the cover 18. According to one embodiment, this close tolerance fit  
passively aligns the FSA to the cradle in the lateral and axial directions, or x and z directions.  
Furthermore, the cradle cover 18, when it comes in contact with the FSA 20, aligns the FSA in  
30      the z direction.

35      Although the foregoing structures have been described with specificity for controlling the  
lateral and axial movements of the FSA 20, and to therefore create a passive alignment between  
the FSA 20 and the connector latch, as further discussed below, variations in the features to  
accomplish same may be achieved without deviating from the scope of the present invention, and

1 are contemplated to fall within the scope of the invention. Among other alternatives, the location  
5 and configuration of the notch and step guide may be varied without undue experimentation.

In a like fashion, two correspondingly positioned guide holes 50 are fabricated near the  
5 peripheral edges of the cradle cover 18. Thus, when the cradle cover 18 is placed over the lower  
cradle 17 and comes to rest thereon, the guide holes 50 and the hold-down apertures 32 coincide  
and are in position to receive a pair of hold-down screws 52.

Referring further to FIGS. 2 and 2A, in this embodiment of the invention, the two-part  
10 optical plate 22 is made of a dielectric upper section 24, such as ceramic, and a metal lower  
section 25, such as stainless steel. Like the lower cradle 17, the lower plate 25 has a generally  
U-shaped configuration. The center "U" section comprises a stepped upper deck 56 and a  
stepped lower deck 58. The stepped upper deck 56 includes a gap passage that resembles a notch  
28 for allowing signals from a bi-directional laser to pass through.

15 In a like but opposite manner, the upper ceramic substrate 24 includes a stepped deck.  
Its upper deck 60 and lower deck 62 coincide with the lower plate's upper and lower decks. Still  
referring to FIG. 2, when the upper substrate 24 and lower plate 25 come in contact and are in  
a mated position, the two lower decks superimpose, and the two upper decks abut each other.  
20 A gap may be provided between the two upper decks of the upper substrate 24 and the lower  
plate 25. This gap would be configured to receive a pair of pinheads 63 and to roughly align the  
cradle assembly (including the FSA 20) to the two-part VCSEL plate 22 before final active  
alignment. The pinheads 63, therefore, would act like a registered key in fixing the two-part  
25 VCSEL plate 22 along a vertical direction with the cradle 16 (see, e.g., FIG. 4).

Referring again to FIG. 2, the FSA 20 comprises a single block having precision holes  
64 formed in the block to retain a plurality of fiber stubs. Each precision hole 64 extending from  
one edge of the FSA 20 over to the other edge and defining an axial bore 66 therebetween. Thus,  
30 the FSA housing includes a plurality of axial bores for receiving a plurality of optical fibers into  
its interior. The described exemplary FSA 20 may be injection molded using a thermoset resin  
to minimize thermal expansion mismatches between the optical interface unit 10 and the OSA  
standardized MT connector. Also, it is understood that the invention is not limited to a specific  
number or range of axial bores.

1        The FSA 20 is confined laterally as it sits between the two-part cradle 16 by a molded  
5        male detent 68, which coincide with the notch 42 on the stepped deck 34. The male detent 68,  
10      therefore, abuts the two steps 36 on either side and is prevented from moving laterally by the  
5        steps. To fix the FSA 20 in the axial direction, the FSA 20 is further molded with a stop member  
10      70. The stop member 70 extends from the base of the FSA 20, and, when positioned in the cradle  
5        16, coincide with the guide 38 on the stepped deck 34. The stop member 70 abuts against the  
10      guide 38 and is prevented from moving axially towards the first mating surface 44. The FSA 20  
5        is prevented from moving away from the cradle along the opposing axial direction by the two-  
10      part VCSEL plate 22.

15      Along the FSA 20 upper surface are two load-bearing members 72. The two load-bearing  
5        members 70 protrude above the FSA's top surface 74. Accordingly, when the FSA 16 is encased  
10      between the two-part cradle 16, the cradle top cover 18 comes in contact with the load bearing  
5        members 70 and not the top 74 of the FSA 20. Hence, when a pair of screws 52 are tightened  
10      against the threaded hold-down apertures 32, compressive force is generated over the two load-  
5        bearing members 72 to thereby secure the FSA 20 within the two-part cradle 16, to therefore fix  
10      the y movement between the cradle 16 and the FSA 20.

20      The FSA 20 further includes a pair of guidepin holes 76. Like the precision holes 64, the  
5        guidepin holes 76 extend from one edge of the FSA over to the opposing edge, which define a  
10      pair of guide collars 78 therebetween. The guide collars 78, the axial bores 64, the front mating  
5        surface 80, and the rear mating surface 82 may be molded in accordance with the IEC 1754-5  
10      standard. As such, when the fibers from a mating conventional MT ferrule are aligned with the  
5        fibers in the FSA 20, the alignment between the various fibers is on the order of 1 micron.

25      The various interface components are assembled in the following manner. First,  
5        individual fibers are inserted and bonded in the precision holes 64 in the FSA 20, typically using  
10      an epoxy such as 353ND from Epoxy technology. The ends are then polished to industry  
5        standard tolerances while simultaneously maintaining the necessary length tolerances that the  
10      particular configuration requires. Next, a pair of guide pins 84 are inserted in the guidepin holes  
5        76 with the pin heads 63 protruding out from the FSA 20. The guide pins are then secured in  
10      place by epoxy. The FSA 20 is then placed onto the lower cradle 17 and is manipulated so that

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1 the male detent 68 rests between the two steps 36 and interposed between the notch 42. A force  
is also exerted on the FSA 20 to move the FSA forward so that the stop member 70 abuts against  
the guide 38. The upper cradle 18 is then lowered over the lower cradle 17 while maintaining  
5 a rough alignment between the guide holes 50 and the threaded hold-down apertures 32. The  
screws 52 are then tightened over the upper cradle with sufficient amount of force to compress  
the load bearing members 72. Next, the MTP/MPO connector latch 14 is fit against the cradle  
halves 17/18 (as further discussed below) and bonded in place. The assembled components are  
10 referred to as an assembled cradle assembly 19.

15 The VCSEL array 12 and the photodiode 26 are mounted on the two-part VCSEL plate  
22 by passive alignment equipment, such as the FINEPLACER® system. An epoxy, such as  
E3001 from Epoxy Technology, may be used to hold the two-part plate 22, the VCSEL 12, and  
the photodiode 26 in place after they have been passively aligned. Other exemplary epoxies such  
as EPO-Tek E3001, Dymax UV Epoxy 9-20274-GEL or similar epoxies, may be used in other  
exemplary embodiments. In some exemplary embodiments, different epoxies may be used for  
the various components of the interface unit. In an exemplary embodiment, Dymax UV Epoxy  
9-20274-GEL may be used to secure the FSA to the cradle or retainer and EPO-Tek E3001 may  
20 be used to secure the VCSEL die and the monitor diode according to the exemplary embodiments  
in which such components are included. The assembled VCSEL plate assembly 27, is then  
placed over and rests on the pinheads 63 which, as discussed above, protrude out from the edge  
of the FSA 20. The assembled cradle assembly 19 and the VCSEL plate assembly 27 are then  
25 ready for active alignment, which is known by persons of ordinary skill in the art as including  
energizing the various components, aligning the fibers with the VCSEL array 12, and monitoring  
the laser output for maximum signal strengths. Once the desired alignment is achieved, the two-  
part cradle is then welded to the lower metal plate 25 by known welding methods, such as with  
30 a YAG laser. Persons of ordinary skill in the art will understand that since the pinheads 63 touch  
the assembled VCSEL assembly 27, the assembled cradle assembly 19 and the VCSEL assembly  
27 are fixed in the Z direction. Thus, during active alignment the assembled components 27 and  
19 only rotate in the X, Y, and theta directions, with respect to each other. Those of ordinary

1 skill in the art will appreciate that many variations or alternatives to the described alignment process may be implemented to achieve the desired degree of alignment.

5 In summary, the optical interface 10 unit accurately terminates the end faces of the fiber stubs relative to two alignment pins 84 that interface with alignment holes on the standardized connector. The VCSEL array 12 may be integrated into a plate assembly 22 having a weldable ceramic plate and a substrate for optimized coupling to the optical interface unit 10.

10 Details of various other optical interface unit embodiments are illustrated in FIGS. 5, 6, and 8-16. Specifically referring to FIGS. 5 and 6, in one embodiment, an FSA 86 comprises a single block having precision holes 88 formed in the block to retain a plurality of fiber stubs. Each precision hole 88 extending from one edge of the FSA 86 over to the other edge and defining an axial bore 90 therebetween. Thus, the FSA housing includes a plurality of axial bores for receiving a plurality of optical fibers into its interior.

15 The described exemplary FSA 86 may be injection molded using a thermoset resin to minimize thermal expansion mismatches between the optical interface unit 10 and the OSA standardized MTP/MPO connector. The FSA 86 may further include a well 92 in the upper surface of the block to dispense epoxy. Epoxy is preferable to secure the fibers in place as this eliminates the need for springs or other retention mechanisms. In addition, the FSA 86 of FIG. 20 5 may include a chamfer 94 on the back surface 96 to interface with the optoelectronic device 12. In other words, the chamfer 94 provides clearance for bond wires. In addition, the front side 100 of the FSA 86 interfaces with standardized connectors and therefore preferably includes an 25 angled surface for optimal coupling with standard ferrules having single mode fibers. In a typical connection with a conventional MTP/MPO connector, this angled surface would be 8° from perpendicular (if a single mode fiber). However, depending on a particular connector, persons of ordinary skill in the art will understand that other angles may be prescribed to achieve a 30 corresponding match without deviating from the scope of the invention, such as zero angle for a multi-mode fiber application. Also, index-matching material such as an optical gel may be used to reduce reflections at the fiber interface. According to one exemplary embodiment, optical gel NYOGEL OC-431A-LVP may be used, but other optical gels may be used in other 35 exemplary embodiments.

1        In the described exemplary embodiments of FIGS. 5 and 6, the precision holes 88 accurately position the end face 96 of the FSA 86 (preferably within about +/- 0.5-1 micron) and a pair of guide holes 98 in accordance with the IEC 1754-5 standard. The single block design  
5        provides high tolerances allowing for the use of the cradle assembly of FIG. 2, in conjunction with laser welding to align the optoelectronic device with the FSA 86.

10       Referring to FIG. 7, there is shown and described an alternate interface unit including a modified FSA 86 that sits in a modified two-part cradle 200. Instead of the stepped deck in FIG. 2, the modified two-part cradle 200 comprises a single layer deck 202. A stop member 204 is configured along one of the edges, next to the second mating surface 46. When the FSA 86 is nestled within the two-part cradle 200, the stop member 204 abuts against the base of the FSA 86 to thereby fix the FSA 86 in the axial Z direction. The modified two-part cradle 200 is configured with the same half-channel 206 as the cradle of FIG. 2. The half-channel 206 extends the perimeter of the cradle opening and acts like a groove for a corresponding tongue (not shown) on the MTP/MPO connector latch 14.

15       The modified FSA 86 has a general shape of a rectangular box except for one of its sides, which slightly slopes to match the angle of the conventional MTP/MPO connector. Unlike the  
20       FSA of FIG. 2, the modified FSA 86 does not have load bearing members, a notch, or a stop member. Also, axial and lateral movements between the FSA 86 and the two-part cradle 200 are performed in a modified fashion as further discussed below.

25       The VCSEL array 12 and photodiode 26 may be assembled to the two-part VCSEL plate 22 and passively aligned as before. However, on the lower plate 25 two axial bores 208 are provided on either side of the notch 28. These axial bores 208 have a circumference that is slightly larger than the circumference of the pinheads 63. This slightly larger circumference functions to permit mating with the guide pins 84 and still provide a rough alignment between the assembled VCSEL unit and the FSA 86. Power is then turned on to actively align the fibers with the VCSEL array 12, as discussed above for final alignment. The cradle is then welded to the lower metal VCSEL plate by known welding methods, such as with a YAG laser. Hence, a gap in the embodiment of FIG. 2 is not required, and, unlike the VCSEL plate of FIG. 4, the two upper decks 56 and 60 touch.

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1        The FSA 86 is fixed in the two-part cradle 200 by first placing the FSA 86 on top of the  
lower cradle 17 over the single layer deck 202. Care is taken to abut the FSA 86 against the stop  
member 204. Epoxy is also applied to the base of the FSA 86 to secure it in place. The cradle  
5        cover 18 is then placed over the lower cradle 17 and a pair of screws inserted and tightened.  
Because the modified FSA 86 does not have any load bearing members, compression force is  
applied directly on the FSA housing, the top surface 87.

10       Referring to FIG. 8 and 9 an alternate embodiment of the present invention includes  
forming the FSA of FIGS. 2 and 7 from two separately molded plastic blocks to aid in the  
manufacturability of the FSA. In this embodiment, the two-part FSA 102 again includes  
precision holes 88 to retain a plurality of fiber stubs that are precisely located relative to the  
guide-pin holes 98. However, in the alternate two-part embodiment 102, the precision holes 88  
15       need not be aligned from one side to the other. Rather, the use of two array blocks allows for  
the alignment of the fiber holes and guide pins with one piece of mold steel for each of the front  
and rear optical surfaces during the molding process. Persons of ordinary skill in the art will  
understand that the two-block design may therefore reduce tooling costs and provide increased  
yields with more accurate precision than the single block design of FIGS. 2 and 7.

20       In addition, each half of the molded block may include a well 92 formed on the upper  
surface to capture any overflow when excess epoxy is used to secure the fibers in place. The two  
half blocks may further include mechanisms to assist in aligning the blocks. For example, a  
25       tongue and groove type mechanism 104 may be included on each of the blocks as shown to  
mechanically align the blocks when bonded together with an epoxy or other bonding materials  
known in the art. Also, because of the well 92, portions of the precision holes are actually half-  
30       circles and not "precision holes."

35       Referring to FIGS. 10 -13, a further alternate embodiment of the FSA 20 of FIG. 2 may  
again be formed from two blocks. In the described exemplary two-part embodiment 106, either  
the inside surface of the upper 108 or lower 110 blocks (or both) include nested V-grooves 112  
to retain a plurality of fibers. For ease of manufacturing the V-grooves 112 may be formed in  
a single surface with the opposing surface being flat to rigidly secure the fibers in the nested  
grooves. When the upper block 108 is superimposed over the lower block 110, the adjoining V-

1 grooves 112 and flat surface form axial bores in the resulting block. As before, two end grooves  
are provided. The end grooves are precisely located relative to the guide-pin holes that are  
designed in accordance with industry accepted standards.

5 Advantageously the use of nested V-grooves having flat side walls facilitates the use of silicon  
grown tooling rather than more expensive metal tooling. The nested V-groove further allows the  
fiber to be rigidly secured relative to the end grooves without the use of springs or other  
secondary retention mechanisms. In addition, the nested V-grooves may register the fiber with  
10 greater accuracy than the cylindrically shaped axial bores of FIGS. 2 and 7. This is because by  
definition, the axial bore must be larger in diameter than the fiber itself in order for the fiber to  
pass through. Thus, this allows for some level of movement / misalignment of the fibers. To  
15 illustrate how the V-grooves 112 enhance alignment, FIG. 13 is a perspective view of the FSA  
106 of FIGS. 10-12 with the upper cover 108 removed. In this figure, a person of ordinary skill  
in the art will understand that the area of the V-grooves 112 allows the fibers to directly register  
20 with the flat V side wall portions of the V-grooves 112 in the molded block. Due to the fiber's  
cross-sections being circular, and that the three points of contact created by the V-groove side  
walls of a V-groove 112 and the upper cover define a circle, the all the fibers are biased to the  
bottoms of the grooves. This is difficult in a circular axial bore arrangement as there is no active  
25 force that pushes the separate fibers to similar positions in the precision holes.

Referring to FIGS. 14-16, in an alternate embodiment, the V-groove design of FIGS. 10-  
13 is further modified to allow the V-grooves and the guide holes to be molded or cast from a  
25 single tool. In particular, the modified FSA 114 further includes V-grooves for the guide pins.  
The passageways for the guide pins extend longitudinally from a back end 116 of the housing  
toward its front 118 through the entire length of the housing. The V-grooves (both for the fibers  
30 and guide pins) may again be formed in a single surface on the same block 122. The opposing  
lower surface of the upper block 120 may again be flat. When the upper block 120 is  
superimposed over the lower block 122, the adjoining V-grooves and flat surface form axial  
bores in the resulting block that are interposed between two end grooves. The end grooves are  
35 precisely located relative to the guide-pin holes and are designed in accordance with industry  
accepted standards. Advantageously the alternate design may allow for the use of open / closed

1 tooling having superior repeatability and reduced costs relative to the design of FIGS. 2 and 7. In addition, the use of a single tool element to form the V-grooves may allow the V-grooves to be more accurately registered relative to the guide holes and precision holes, as previously  
5 discussed.

10 Referring to FIGS. 17-19, there is shown yet another interface embodiment 124, which includes a one-piece retainer 126, a modified snap connector 128, and a retainer wedge 130 to wedge an FSA 132. The tongue and groove in this embodiment has been reversed. Accordingly, the retainer 126 has a continuous tongue 134 along a first mating surface 136 for alignment with a corresponding groove or channel (not shown) in the snap connector 128. In the embodiment of FIGS. 17-19, a notch is not used to fix the FSA 132 laterally. Instead, the one-piece retainer 126 uses a combination of registered side wall and retainer wedge 130 to fix the x-y direction and a similar notch and epoxy to fix the axial direction.

15 Referring more particularly to FIGS. 17 and 20, the one-piece retainer has a generally rectangular opening 138 which defines a cavity therein for receiving the FSA 132. Just slightly in from the opening 138 and axially removed from the first mating surface 136, there is shown a sloping side wall 140 and a raised floor 142. As further discussed below, the sloping side wall 140 has a slope that is identical or approximate to that of a side wall on the FSA 132. The sloping side wall 140 runs continuously from a first starting position near the first mating surface 136 to a second position towards a second mating surface 146. Accordingly, when the FSA 132 is slidably positioned in the one-piece retainer 126 and the wedge 130 is inserted, the two sloping  
20 surfaces (of the retainer and of the FSA) coincide and abut to restrain the FSA from lateral movement with respect to one another.

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30 The raised floor 142 extends approximately the width of the opening 138 and the depth of the one-piece retainer 126. As indicated in FIGS. 20 and 21, a notch 144 at the tip of the raised floor along the back side is provided, opposite the side with the tongue 134, near the second material surface 146. This notch 144 is configured to stop the FSA 132 from moving any closer to the VCSEL array when the various components are mechanically and electrically coupled together, thus fixing the gap between the FSA and the VCSEL array.

1 Several apertures are provided in the one-piece retainer 126. A connector threaded  
retaining aperture 148 is configured on the first mating surface, just above the opening 138, and  
provides a gripping surface for a screw. As understood from FIGS. 17 and 19, this threaded  
5 aperture is partly responsible for fixing the snap connector 128 to the one-piece retainer 126.  
Two other apertures are a wedge well 150 and a gripping well 152. The wedge well 150 extends  
through the entire height of the one-piece retainer 126 and partially intersects the cavity along  
the non-sloping surface side wall of the retainer 126. The shallow gripping well 152 is beveled  
10 and is provided so that the retainer is easily gripped by the alignment tooling as the components  
are actively aligned. As indicated in FIG. 20, the gripping well 152 does not extend through into  
the cavity region and is preferably centrally located along the top of the one piece retainer  
adjacent the wedge well and terminates directly over the threaded aperture 148. Two enlarged  
15 cut-outs 145 in the central cavity of the retainer 126 are shown. These enlarged cut-outs 145 are  
included to relief the cutter when the cutter is used to create the cavity during the manufacturing  
process. However, they are not required if other manufacturing steps are employed.

Referring to FIGS. 22-24, there is shown and described a retainer wedge 130. The  
retainer wedge 130 may be made of the same material as the one-piece retainer (e.g., a weldable  
20 metal such as stainless steel). The retainer wedge is rod-like in shape and is tapered lengthwise  
along one direction 154. The wedge 130 includes a cut section 156 along the arch circle and in  
the lengthwise direction. In the same cut region, the wedge is also tapered inward 158. At the  
25 end of the tapered section, the cut region also includes a beveled surface 160 to allow for easy  
passage over the FSA 132 as the wedge is inserted into the wedge well 150. Referring again to  
FIG. 17, there is shown and described a modified MTP/MPO connector latch 162. As before,  
the MTP/MPO connector latch 162 includes a recessed section (not shown) which corresponds  
30 to the tongue 134 on the one-piece retainer 126 and fits with the tongue 134 in a tongue and  
groove fashion. The modified MTP/MPO connector latch 162 also includes a pair of latching  
arms 164 as before to latch with tabs or other detents in the conventional mating MTP/MPO  
connector/ferrule (not shown). The modified MTP/MPO connector latch 162 further includes  
a notch 166 along the upper flange 168. This notch 166 is in-line with the threaded aperture 148

1 as the latch and the retainer are mated and allows a screw 170 to pass through to fasten the  
MTP/MPO connector latch to the retainer.

5 The FSA 132 in FIGS. 17, 25 and 26 is similar to the FSA in FIGS. 2 and 5 with some  
exceptions. First a pair of round wells 172 are provided to relieve excess epoxy as epoxy is  
10 applied to fasten the guide pins into the guide holes. Second, the guide pins do not extend  
beyond or out of the FSA along the back surface 174. This is partly due to the way the  
retainer/FSA combination is aligned to the VCSEL plate, as further discussed below. In addition  
15 to a tapered front surface 178 for mating with a tapered conventional MTP/MPO ferrule for a  
single mode application, the back surface 174 is also tapered along the back surface upper region  
20 179. This tapered back upper region 179 is configured to allow clearance for wire bonding. The  
side is also tapered 181. This taper has the same slope as the wedge slope 158 and the sloping  
side wall 140 for a close fit.

15 Referring to FIGS. 18 and 27, the two part VCSEL plate assembly, as before, includes  
a lower metallic VCSEL plate 182 and an upper ceramic substrate 184. In part for EMI  
protection, the ceramic substrate is further configured with a ground plain 186 which provides  
20 both electromagnetic shielding and electrical grounding for the VCSEL array. The ceramic  
substrate 184 is shown with a flex circuit 188 and is generally provided to couple the OSA to a  
PC board or other electronic substrates.

25 Still referring to FIGS. 18 and 27, the flex circuit may be wire bonded to the ceramic  
substrate via traces embedded in the substrate. The flex circuit 188 in this embodiment contains  
coplanar transmission lines. The coplanar transmission line based flex circuit preferably provides  
30 high speed characteristics while being thinner than conventional flex circuits. Due to its  
relatively small thickness, the coplanar transmission line based flex circuit may result in smaller  
bending radius when bent for coupling to the PC board or the like. This reduced bending radius  
may then result in reduced signal distance between the lasers and the PC board and theoretically  
35 leads to better signal performance.

As before, passive alignment between the VCSEL array, photodiode, ceramic substrate,  
and VCSEL plate to produce a VCSEL plate assembly is performed by prior art methods such  
as pick and place using the FINEPLACER® system. Referring to FIG. 17, passive alignment

1 between the one-piece retainer 126, the FSA 132, and the MT connector latch 162 may be  
performed in the following fashion. First, the FSA 132 is inserted into the cavity from the first  
mating surface 136. The FSA 132 is pushed back until it buts against the notch 144. (See in  
5 addition FIG. 20.) The wedge 130 is then inserted into the wedge well 150 with the cut surface  
158 facing the FSA 132. A set screw 131 is then placed into the well and tightened. As the set  
screw 131 is rotated, it imparts pressure to the wedge 130, which in turn pushes against the side  
of the FSA 132. Through translation, the FSA 132 is biased against the sloping side 140 of the  
10 one-piece retainer 126. Epoxy is then applied to the FSA 132 to fix the FSA in the axial  
direction. The assembled FSA and retainer is referred to as a retainer assembly component.

Passive alignment between the MTP/MPO connector/MT ferrule and the retainer  
assembly component is achieved by sliding the MTP/MPO connector latch 162 over the tongue  
134 to register in a tongue and groove fashion. The hold down screw 170 is then tightened by  
sliding the tip of the screw past the notch 166 located at the connector flange 168 and into the  
15 threaded aperture 148. Next, a conventional connector/ferrule is inserted and snaps with the  
MTP/MPO connector latch 162. The MTP/MPO connector latch 162 is configured to slide the  
conventional connector/ferrule through conventional registration 165. As the MTP/MPO  
20 connector slides forward to a final gripped position, the two guide holes on the MT ferrule  
engage the pair of guide pins 84 on the FSA 132. As the conventional connector/ferrule is further  
slid into the MTP/MPO connector latch, the close tolerance between the guide pins 84 and the  
25 guide holes on the conventional MT ferrule provide the final alignment. As previously discussed,  
this final passive alignment between the fibers in the conventional connector and the fibers in the  
FSA 132 is within +/- 0.5 to 1 micron.

The final alignment between the VCSEL plate assembly and the retainer assembly  
component is performed by active alignment. This is accomplished by powering up the lasers  
30 and emitting signals to the fibers. At the same time, the retainer assembly component and/or  
VCSEL plate assembly is manipulated in the x, y and theta directions (theta is the rotation  
between the x-y plain), and signal strength is monitored. Once maximum signal strength is  
achieved, the retainer to the VCSEL plate is welded with known welding methods, such as with  
a YAG laser. The entire interface unit is now globally aligned. Hence, when the embodiment  
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47075/SAH/C715

1 of FIG. 19 (and the various other embodiments) is used in the field, all that is required is to insert  
5 a conventional MTP/MPO connector for a satisfactory alignment.

Although the passive alignment embodiment in FIGS. 17 and 18 is described with  
5 particularity, other alignment arrangements are contemplated and are considered to fall within  
the scope of the present invention. This includes switching the sloping side for the other side  
wall, changing the notch to locate near the second mating surface, and providing a raised floor  
with a different configuration, just to name a few.

10 Referring to FIG. 28 yet another alternative embodiment is illustrated. In this  
embodiment, the ceramic substrate of FIGS. 18 and 27 is exchanged for a metal backing plate  
190, which may be made of a weldable metal such as stainless steel. The backing plate 190 has  
no conductive traces, and accordingly, the flex circuit 188 is directly coupled, both mechanically  
and electrically, to the photodiode 26 and the VCSEL array 12 through wire bond methods.  
15 Thus, signal distance is further reduced from the embodiment in FIG. 18 and 27 due to fewer or  
shorter traces. As discussed above, this should theoretically lead to better signal performance.

20 Still referring to FIG. 28, the VCSEL plate 182 is the same as before (see, for example,  
FIGS. 18 and 27) and includes the same notch 28 for signal transmission from a bi-directional  
VCSEL array to pass through. The backing plate 190 has a configuration that resembles a  
25 rectangular block. However, instead of having perfectly square edges, the backing plate 190 has  
a taper surface 192 on one of its sides. This taper surface 192 allows the flex circuit 188 to bend  
and couple to a PC board or other electrical substrates while minimizing the distance of the flex  
circuit and traces on the ceramic substrate. Thus, this should theoretically lead to better signal  
30 performance.

35 FIG. 29 is still yet another alternative embodiment. In this embodiment, the retainer has  
been eliminated to further reduce the number of components involved. In one embodiment, the  
interface unit 210 includes a metallic base unit or pin plate 212, a weld plate 214, a ceramic  
substrate 216, a monitor diode 26 and VCSEL array 12, an FSA 218, and a modified MTP/MPO  
connector latch 220. The base unit or pin plate 212 may be made of a weldable material such as  
stainless steel and resembles two integrated plates at a right degree angle. However, a solid  
rectangular block and other angles are also contemplated depending on the particular application.

1        The horizontal section 222 includes a reinforcement member 224 for reinforcing the joint  
between the horizontal section 222 and the vertical section 226. However, no reinforcement is  
contemplated where the application has little or no exertion force. Two guide pins 84 are pressed  
5        fit into a pair of guide holes 228 along the vertical section 226 of the pin plate 212. As further  
discussed below, these guide pins provide a coarse alignment between the VCSEL array 12 and  
the optical fibers, and a finished passive alignment for the FSA 218 and the conventional  
connector/ferrule.

10      Among several modifications, the embodiment of FIG. 29 reverses the order of the  
ceramic substrate 216 and the weld plate 214. Unlike the embodiments of FIGS. 2, 7 and 18, the  
VCSEL array 12 is bonded to the ceramic substrate 216 and not the weld plate 214. The ceramic  
substrate 216 includes an overhang section or a ledge 230. The ledge is configured to sit and rest  
over the top surface 234 of the weld plate 214. In the rested position, a pair of oversized  
15      alignment holes 236 on the weld plate 214 match and coincide with a similar pair of oversized  
alignment holes 238 on the ceramic substrate. The two pairs of oversized alignment holes 236  
and 238 are considered oversized when viewed with respect to the diameter of the guide pins 84.  
In other words, the guide pins 84 and the oversized alignment holes are in a loose fitting  
20      arrangement, unlike the fit between the guide holes 228 on the base unit and the guide pins 84.

25      As discussed above, the VCSEL array 12, the photodiode 26, the ceramic substrate 216,  
and the weld plate 214 are first passively aligned and bonded using an alignment device such as  
the FINEPLACER® system. The bonded and aligned components, also referred to as a VCSEL  
plate assembly, are then coupled with the pin plate 212 via passing the guide pins 84 through the  
alignment holes 236 and 238. The FSA 218 is then slid over the guide pins 84 and placed  
adjacent the VCSEL plate assembly. Like before, this provides a rough alignment between the  
VCSEL array and the fibers in the FSA 218 in the X, Y and theta directions.

30      The modified MTP/MPO connector latch 220 is then mounted over the pin plate 212.  
This is accomplished by providing a pair of connector guide holes 240 along the opposing ends  
of the lower edge of the pin plate 212. Regarding the modified MTP/MPO connector latch 220,  
a pair of placement pins 242 and a pair of latch arms 244 along the two edges of the connector  
flange 246 are provided. Unlike a tongue and groove arrangement of FIGS. 2 and 7, the present  
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1 embodiment uses the combination of placement pins 242 and latch arms 244 to connect to the  
pin plate 212, and uses no tongue or groove on the flange 246. The latch arms 244 include a  
5 male detent 248 on each arm. Each male detent is configured to deflect as the MTP/MPO  
connector 220 is inserted over the pin plate and to spring back and grip the sides of the vertical  
section 226.

10 Active alignment is performed by connecting a fiber array jumper with a modified MT-  
like ferrule to the guide pins. This alignment ferrule enables alignment while not crushing any  
15 wirebonds. Signal strength is then monitored at the other end of the fibers while the VCSEL  
plate assembly is manipulated about the loose fitting oversized alignment holes 236 and 238.  
Once maximum signal strength is achieved, the alignment is captured by permanently welding  
the weld plate 214 to the pin plate 212. The alignment ferrule is then removed and replaced by  
the FSA which is then bonded in place.

15 FIG. 30 is yet another alternative embodiment of an interface unit provided in accordance  
with practice of the present invention. As in the embodiment of FIG. 17, the present exemplary  
interface unit 250 comprises a modified one-piece retainer 252, a modified snap connector 254  
20 (also sometime referred to as a connector latch), and a wedging feature for securing and aligning  
the FSA 132. In more detail, the modified one-piece retainer 252 utilizes a pair of alignment  
holes 256, 258 and a female detent 260 in lieu of a tongue 134 design of FIG. 17. As further  
discussed below, the pair of alignment holes 256, 258 allow the modified snap connector 254 to  
25 align itself with the one-piece retainer 252 through a pair of mating alignment pins 262 (FIG. 31).  
In addition, the female detent 260 is configured to receive the connector detent 264 (FIG. 31)  
to therefore further removably secure the snap connector to the one-piece retainer.

30 In an exemplary embodiment, one of the pair of alignment holes 256, 258 is machined  
with a generally oval shape aperture 266 and the other alignment hole is machined with a  
generally circular aperture 268. This may be provided, for instance, to minimize machining  
precision requirement between the centerlines of the two alignment holes 256, 258 with respect  
35 to the alignment pins 262. Accordingly, when the modified snap connector 254 is mechanically  
coupled to the one-piece retainer 252, the centerlines between the two alignment pins 262 can  
vary slightly with respect to the centerlines of the alignment holes 256, 258 without inhibiting

1 the snap connector's ability to couple with the one-piece retainer 252. Alternatively, the  
generally oval aperture and the generally circular aperture may be switched so that the generally  
oval aperture is located on the right side and the generally circular aperture is on the left side  
5 (when view from the perspective of FIG. 30). However, where precision is demanded, the pair  
of alignment holes 256, 258 may both instead be machined with circular apertures.

10 Referring to FIG. 30 in addition to FIG. 31, the female detent 260 is located just below  
the central opening 270 on the one-piece retainer 252. This location coincides with the connector  
15 detent 264 on the snap connector 254, and, accordingly, is configured to receive the connector  
detent 264 when the snap connector is mechanically coupled to the one-piece retainer 252.

15 As with the one-piece retainer in FIG. 17, the central opening of the one-piece retainer  
252 defines a passage 272 in which the FSA 132 may be received. The passage 272 contains  
20 essential features that are similar to the one-piece retainer 126 of FIG. 17, including the sloping  
side wall 140, the raised floor 142, the notch 144 for fixing the Z gap between the FSA 132 and  
the conventional MTP/MPO connector, the wedge well 150, and the gripping well 152. In  
addition, the one-piece retainer has a similar first mating surface 136 and a second mating surface  
25 146. However, in an exemplary embodiment, the retaining aperture 148 on the one-piece retainer  
252 has been modified to receive the fastener 170 in a slightly different fashion. The retaining  
aperture 148 is configured to allow the fastener 170 to pass through when the fastener is inserted  
starting from the second mating surface 146, through the first mating surface 136, and to a  
receiving threaded locking hole 274 on the snap connector 254, where the fastener 170 may be  
30 tightened to removably secure the one-piece retainer 252 with the snap connector 254. Among  
other things, the modified retaining aperture arrangement permits modification to the snap  
connector 254. In an exemplary embodiment, the top 276 of the snap connector 254 is modified  
to include keyway 278 for orientation of the mating MTP/MPO connector. Among other things,  
this keyway 278 ensures correct fiber-to-source/detector connection (e.g., fiber 1 to laser 1 and  
fiber 2 to laser 2).

35 Referring again to FIG. 30, and more specifically to the FSA 132 in FIG. 30. The FSA  
132 is provided with a notch 280. Thus, when the FSA is inserted in the one-piece retainer 252  
and aligned as discussed above for the embodiment in FIG. 17 (i.e., aligned by fixing the side of

1 the FSA with the wedge 130 and then performing passive and active alignment), epoxy may be  
added, which would then flow into the notch 280 and then cured. In effect, the notch 280 acts  
like a keyway and the epoxy like a key when cured to secure the FSA 132 within the one-piece  
5 retainer 252.

10 Referring to FIG. 32, the assembled, aligned, and welded (i.e., the VCSEL plate  
subassembly 282 is welded to the second mating surface 146 after global alignment is performed,  
which may alternatively be secured by epoxy instead of welding as previously discussed)  
15 interface unit 152 is depicted in a 180 degree rotation from the perspective of FIG. 30. The  
passage for adding epoxy into the notch 280 is via wedge well 150, which, as previously  
discussed for FIG. 17, extends the entire height of the one-piece retainer 252. Because it extends  
the entire height of the one-piece retainer, the wedge well 150 is well-suited for accepting epoxy  
20 and allowing the epoxy to flow to the various crevices within the passage 272.

25 To further secure the FSA 132 within the one-piece retainer 252, in an exemplary  
embodiment, additional passages for adding epoxy may be machined in the one-piece retainer  
252, such as epoxy access hole 284. Like the wedge well 252, the epoxy access hole 284 defines  
a passage which flows into the main passage 272 in the central opening 270. Thus, if and when  
20 epoxy is added, epoxy may flow to the various crevices to further secure the FSA within the one-  
piece retainer.

30 As for material selections, although stainless steel was disclosed as an exemplary material  
for the cradle and retainer, among others, and ceramic for part of the VCSEL plate subassembly,  
material selections may be based on the coefficients of thermal expansion of the various  
35 components, including the FSA, the ceramic plate, the guide pins, and the retainer. Generally  
speaking, the coefficient of thermal expansion for the ferrule may be helpful in establishing the  
material selections for the various components of the optical interface unit. For a typical or  
conventional ferrule per industry standard, the following exemplary materials may be used:  
Valox 420 SEO, 30% glass filled PBT for the snap connector; a silica filled thermoset base for  
the FSA; 17-4PH/H1150 SST for the VCSEL plate, the wedge, and the retainer; 420 S.S. for the  
guide pins; and LTCC for the ceramic plate. Such materials are exemplary only and it is also  
envisioned that other materials with similar or substantially equivalent coefficients of thermal  
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1 expansion are available and therefore may be used in implementing the various embodiments of the invention disclosed herein. Accordingly, these alternate material selections are understood to fall within the scope of the invention.

5 It should be understood that the foregoing embodiments are exemplary only and that the present invention includes various other configurations which allow for passive alignment in at least one direction or orientation and active alignment in the remaining directions or orientations. Various mechanical stops or keys may be used to restrict the relative motion between the various 10 components once they are engaged and globally aligned and before active alignment. The present invention covers substrate and subassemblies including additional or fewer components than shown in the various exemplary embodiments, including a VCSEL plate subassembly without monitor diode. In addition, various monitoring techniques may be used which provide a monitor 15 capable of receiving a proportionate fraction of emitted light from data lasers or extra lasers which may emit in one or both of opposed directions. Furthermore, while the invention is disclosed with specificity for a VCSEL array, the same design may be used for other optoelectronic devices such as receivers and transceivers.

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